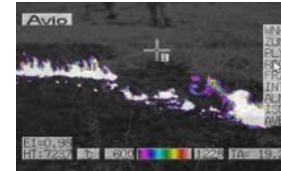
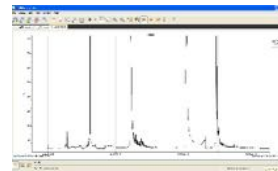


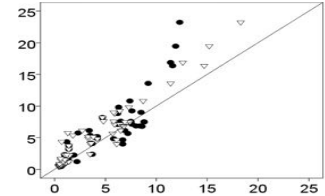
Forest Fire Model Validation

Davide Ascoli (Università di Napoli Federico II)
Elisa Guelpa (Politecnico di Torino – Dip. Energia)
Vittorio Verda (Politecnico di Torino – Dip. Energia)



Objectives of fire field experiments

1. Collect fire behaviour data to **calibrate** and **validate** fire behavior models
2. Test **equipments** used during fire fighting (e.g., protection dispositives, fire shelter)
3. Assess **building flammability** at the Wildland Urban Interface
4. Correlate fire behavior to **ecological** fire effects (e.g. emissions, tree mortality)
5. Others objectives (e.g. fire operators risks, train firefighters...)



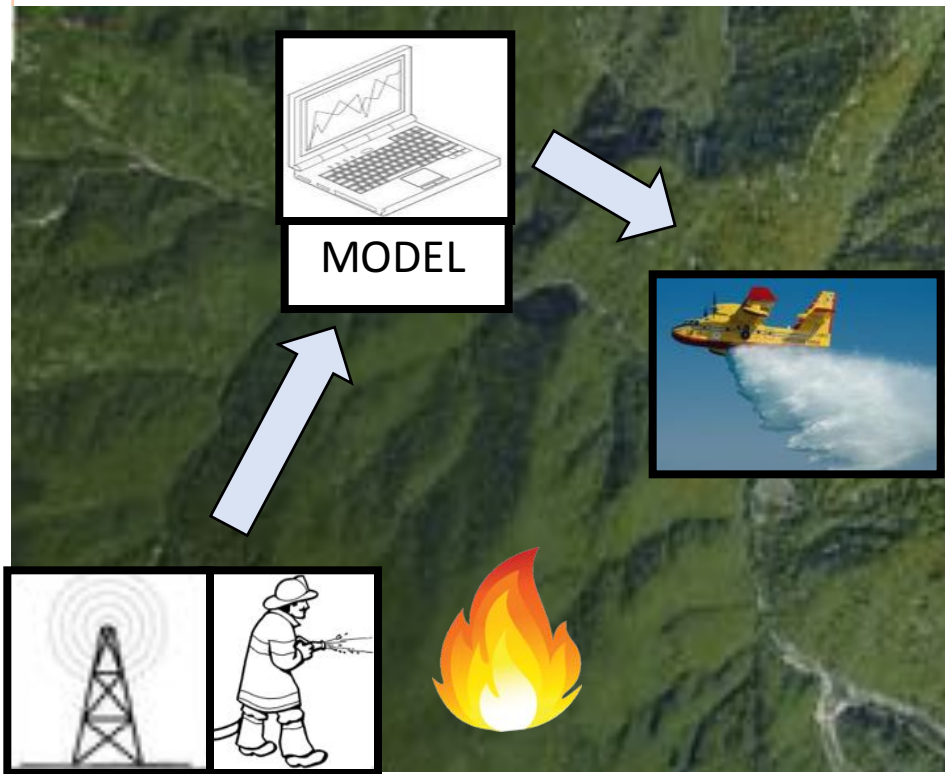
Summary



1. Why fire evolution modelling
2. Experimental data
3. Empirical model validation through experimental data
4. Physical model validation through experimental data

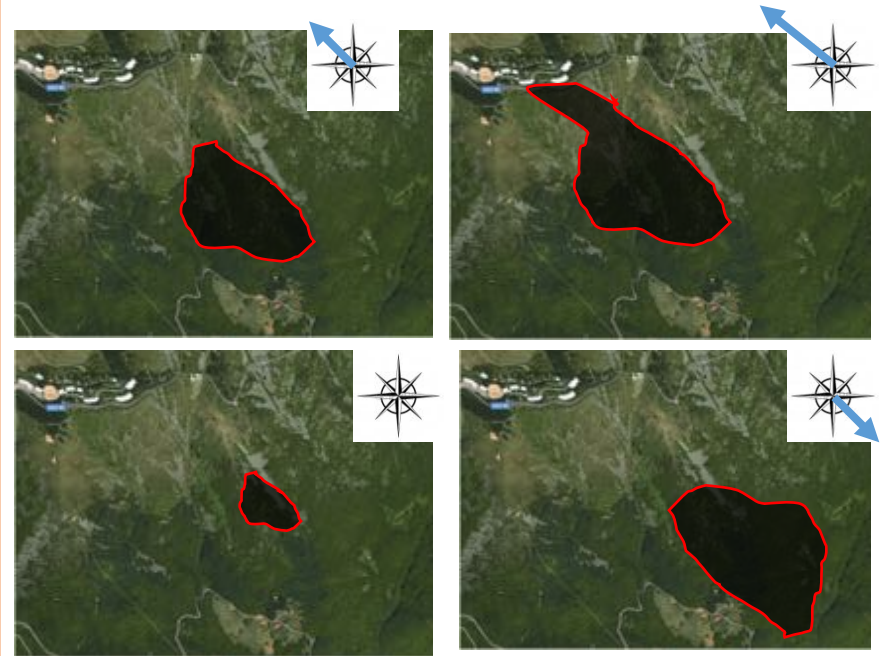
Possible uses of models in operation

FAST SIMULATION MODEL DURING FIRE EVENTS



DETERMINISTIC APPROACH

MULTI-SCENARIO STOCHASTIC MODEL



PROBABILISTIC APPROACH

Information available from modeling

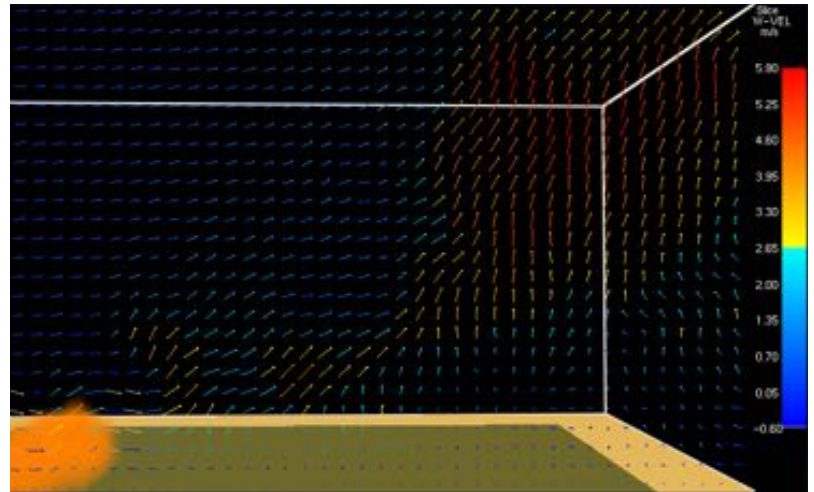
- Optimize the resources for fire extinction (fire fighters, canadair).
- Carry out evacuation plans and reduce fire fighters risk.
- Reduce risk and improve effectiveness payload delivery.

Models for prediction of:

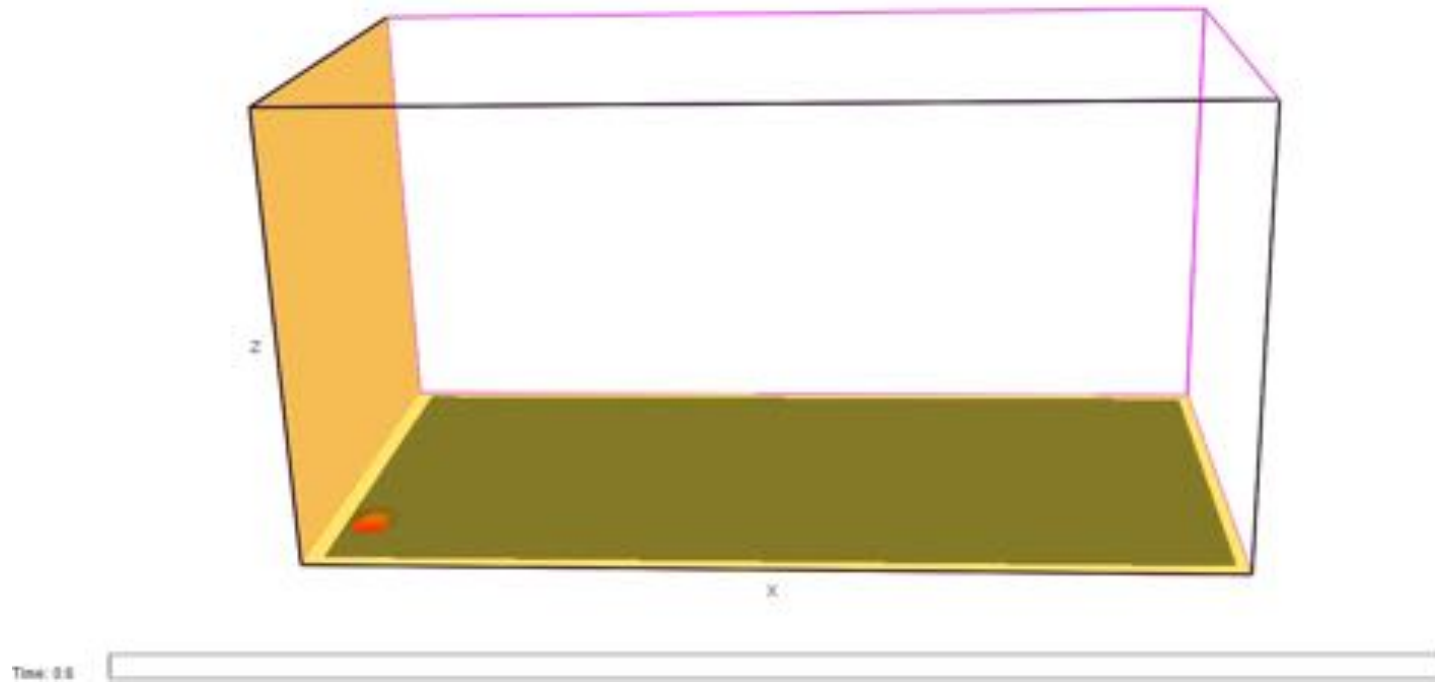
FIRE FRONT EVOLUTION



EFFECTS OF FIRE ON THE SURROUNDING ATMOSPHERE



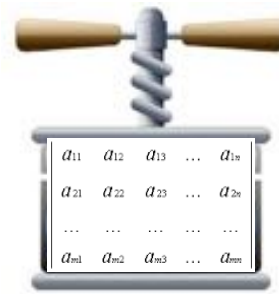
Physical Models



- PROVIDES LARGE AMOUNT OF INFORMATION
- QUITE ACCURATE IF INPUT IS ACCURATE
- TOO SLOW AS MANAGEMENT TOOLS

Are there reasonable ways
to make wildfire physical
models suitable for fast
simulations?

An option is
model reduction



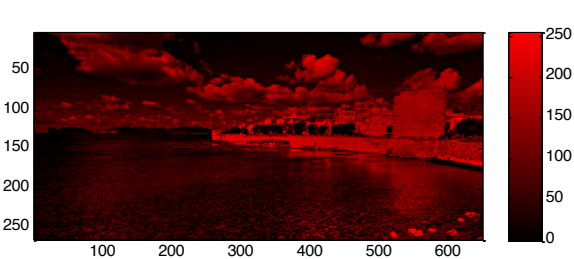
Physical Models

How much information do we need
in order to obtain the main features of a matrix?



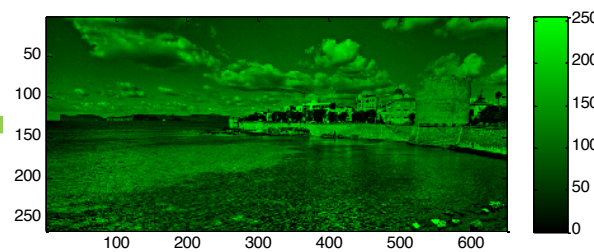
COLORED IMAGE = MATRIX
obtained as a sum of
three matrices

$$A = \begin{pmatrix} a_{11} & a_{12} & a_{13} & a_{14} & a_{15} & \dots & a_{1n} \\ a_{21} & a_{22} & a_{23} & a_{24} & a_{25} & \dots & a_{2n} \\ a_{31} & a_{32} & a_{33} & a_{34} & a_{35} & \dots & a_{3n} \\ a_{41} & a_{42} & a_{43} & a_{44} & a_{45} & \dots & a_{4n} \\ a_{51} & a_{52} & a_{53} & a_{54} & a_{55} & \dots & a_{5n} \\ \dots & \dots & \dots & \dots & \dots & \dots & \dots \\ a_{n1} & a_{n2} & a_{n3} & a_{n4} & a_{n5} & \dots & a_{nn} \end{pmatrix}$$



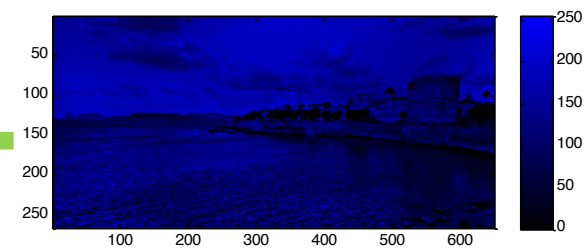
Matrix R

$$A = \begin{pmatrix} a_{11} & a_{12} & a_{13} & a_{14} & a_{15} & \dots & a_{1n} \\ a_{21} & a_{22} & a_{23} & a_{24} & a_{25} & \dots & a_{2n} \\ a_{31} & a_{32} & a_{33} & a_{34} & a_{35} & \dots & a_{3n} \\ a_{41} & a_{42} & a_{43} & a_{44} & a_{45} & \dots & a_{4n} \\ a_{51} & a_{52} & a_{53} & a_{54} & a_{55} & \dots & a_{5n} \\ \dots & \dots & \dots & \dots & \dots & \dots & \dots \\ a_{n1} & a_{n2} & a_{n3} & a_{n4} & a_{n5} & \dots & a_{nn} \end{pmatrix}$$



Matrix G

$$A = \begin{pmatrix} a_{11} & a_{12} & a_{13} & a_{14} & a_{15} & \dots & a_{1n} \\ a_{21} & a_{22} & a_{23} & a_{24} & a_{25} & \dots & a_{2n} \\ a_{31} & a_{32} & a_{33} & a_{34} & a_{35} & \dots & a_{3n} \\ a_{41} & a_{42} & a_{43} & a_{44} & a_{45} & \dots & a_{4n} \\ a_{51} & a_{52} & a_{53} & a_{54} & a_{55} & \dots & a_{5n} \\ \dots & \dots & \dots & \dots & \dots & \dots & \dots \\ a_{n1} & a_{n2} & a_{n3} & a_{n4} & a_{n5} & \dots & a_{nn} \end{pmatrix}$$



Matrix B

$$A = \begin{pmatrix} a_{11} & a_{12} & a_{13} & a_{14} & a_{15} & \dots & a_{1n} \\ a_{21} & a_{22} & a_{23} & a_{24} & a_{25} & \dots & a_{2n} \\ a_{31} & a_{32} & a_{33} & a_{34} & a_{35} & \dots & a_{3n} \\ a_{41} & a_{42} & a_{43} & a_{44} & a_{45} & \dots & a_{4n} \\ a_{51} & a_{52} & a_{53} & a_{54} & a_{55} & \dots & a_{5n} \\ \dots & \dots & \dots & \dots & \dots & \dots & \dots \\ a_{n1} & a_{n2} & a_{n3} & a_{n4} & a_{n5} & \dots & a_{nn} \end{pmatrix}$$

Reduced Physical Models

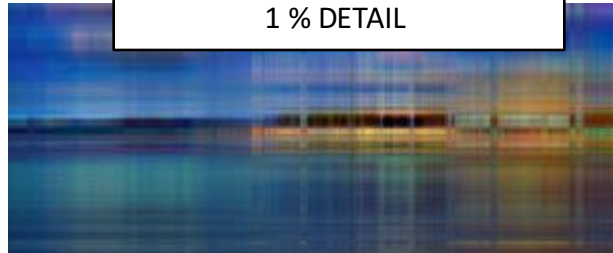
How much information do we need
in order to obtain the main features of a matrix?



0,5 % DETAIL



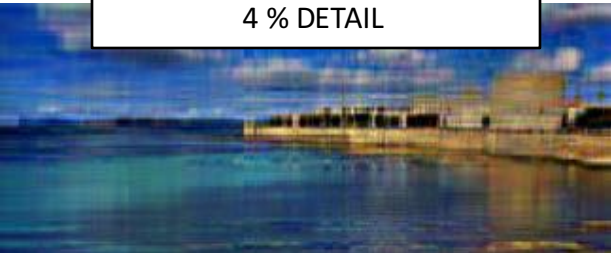
1 % DETAIL



2% DETAIL



4 % DETAIL



7,5 % DETAIL



10% DETAIL



20% DETAIL



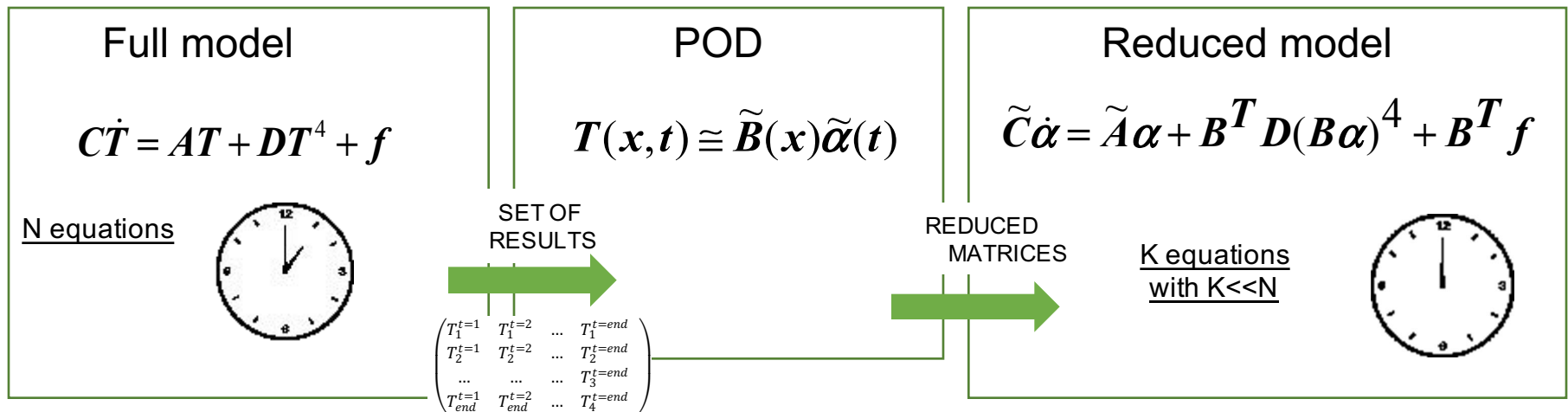
40% DETAIL



100% DETAIL



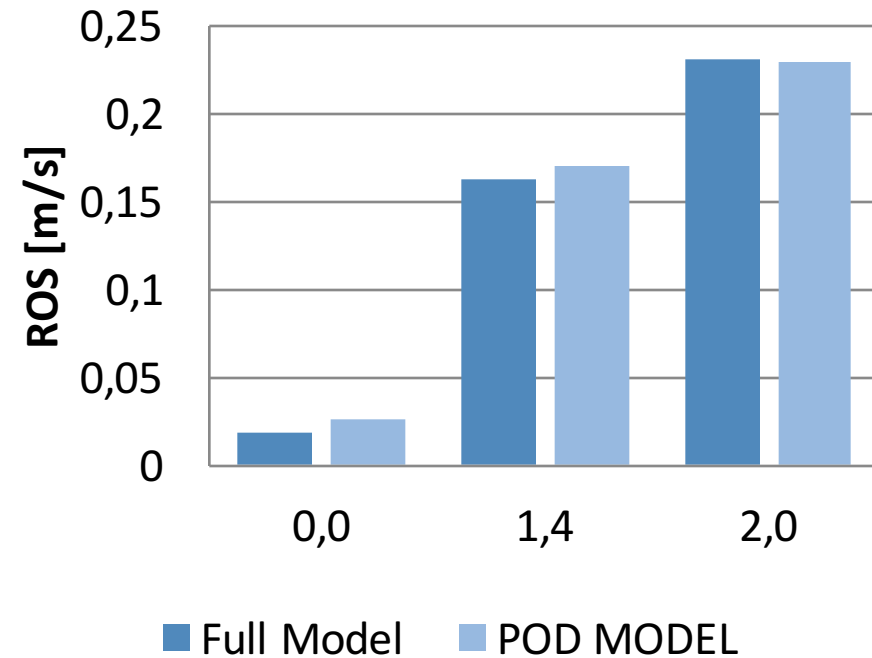
Reduced Physical Models



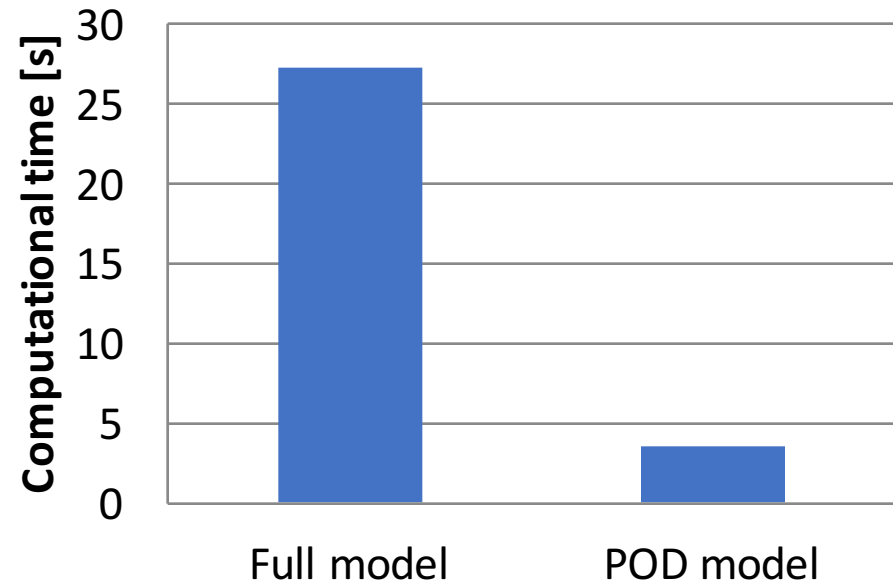
**- 85% of the
computational cost**

Reduced Physical Models

ROS COMPARISON



COMPUTATIONAL COST COMPARISON



Summary

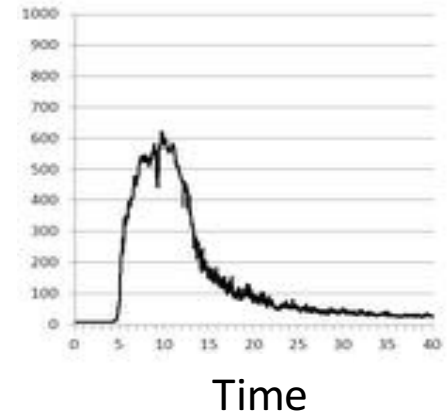
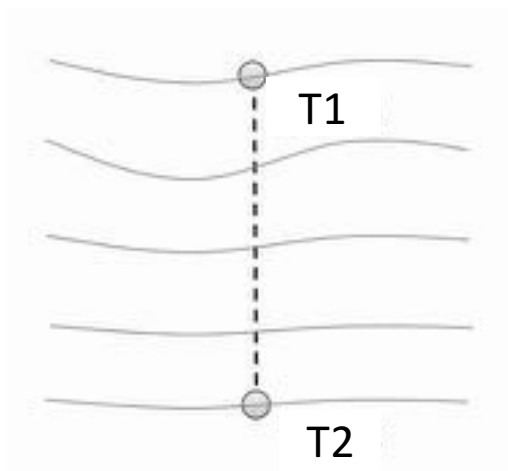


1. Why fire evolution modelling
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What to measure?

Fire descriptors

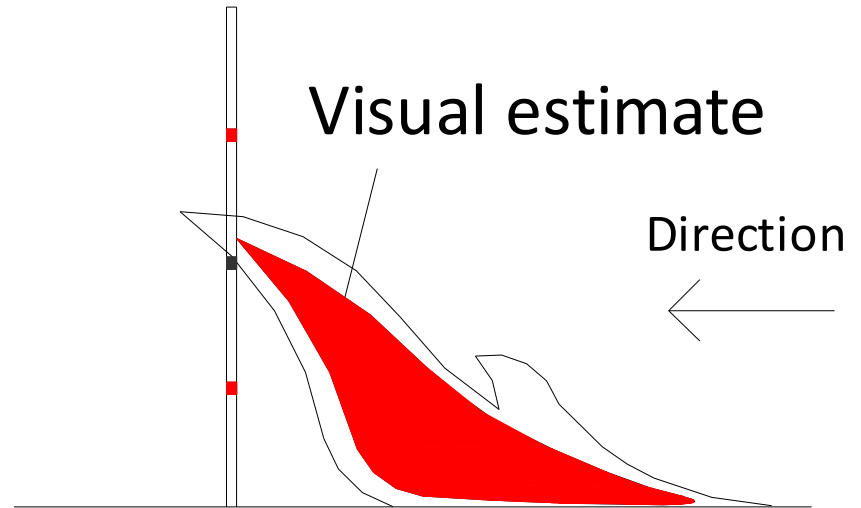
- Flame length (m)
- Rate of spread head, back, flank of the fire front (m/min)
- Fireline intensity (kW/m)
- Fire temperature ($^{\circ}\text{C}$)
- Radiant energy fluxes (kW/m^2)



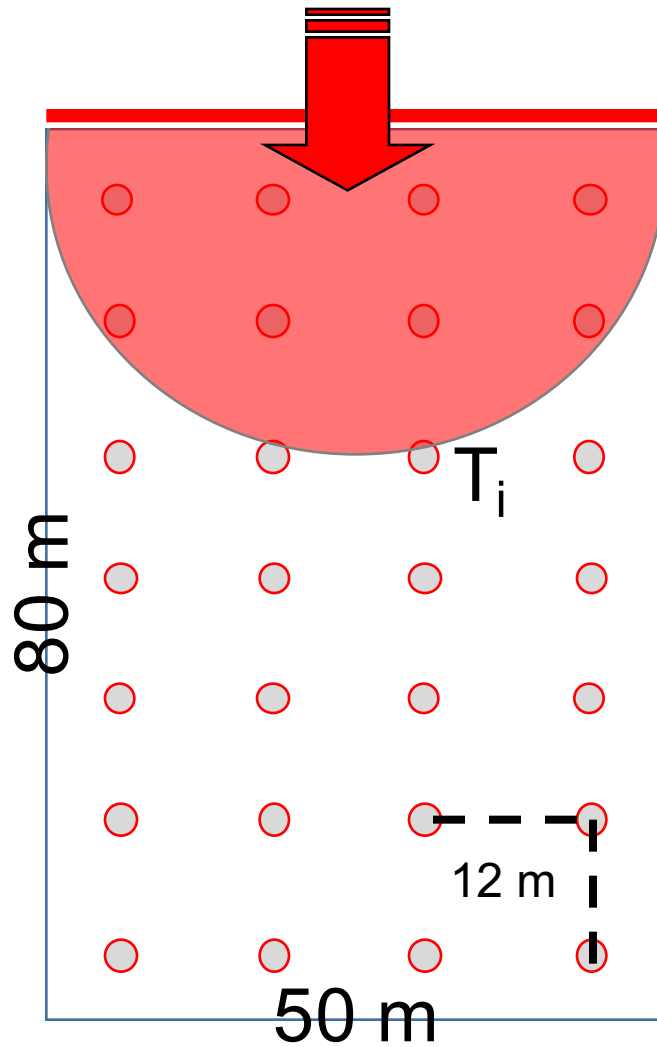
Flame length



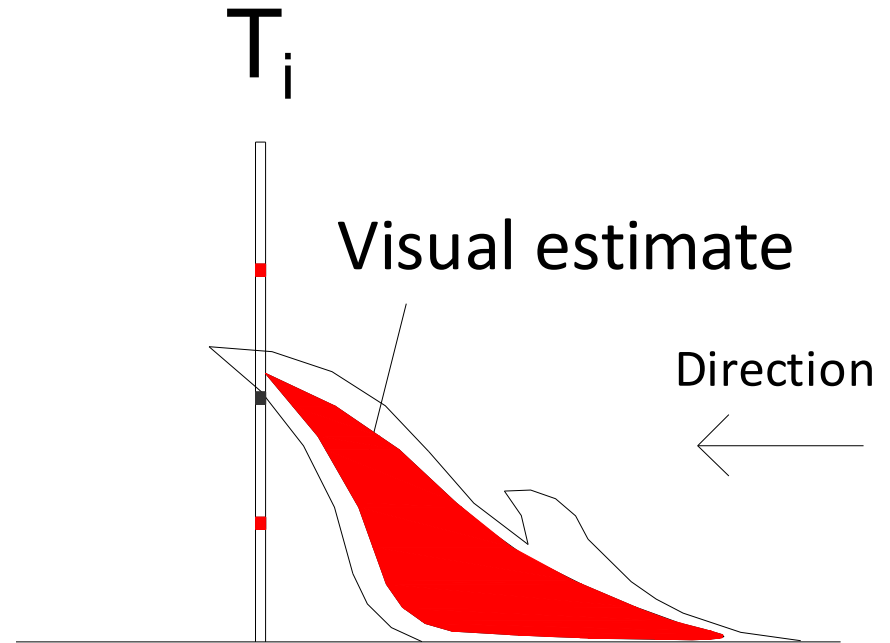
Flame length is the distance from the **average flame tip** to the **middle of the flaming zone** at the base of the fire.



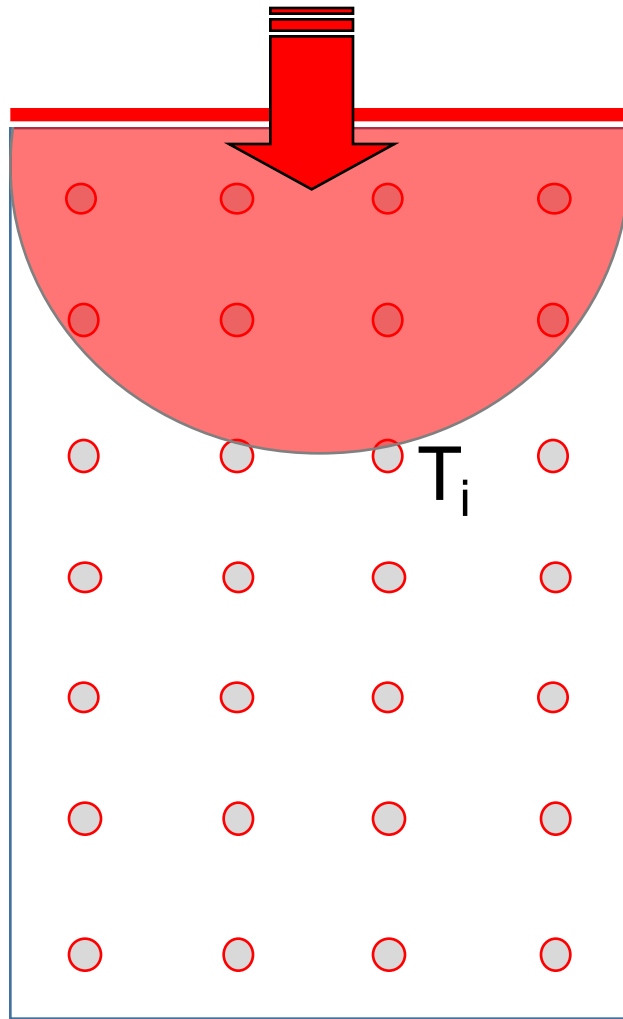
Rate of spread: visual estimate



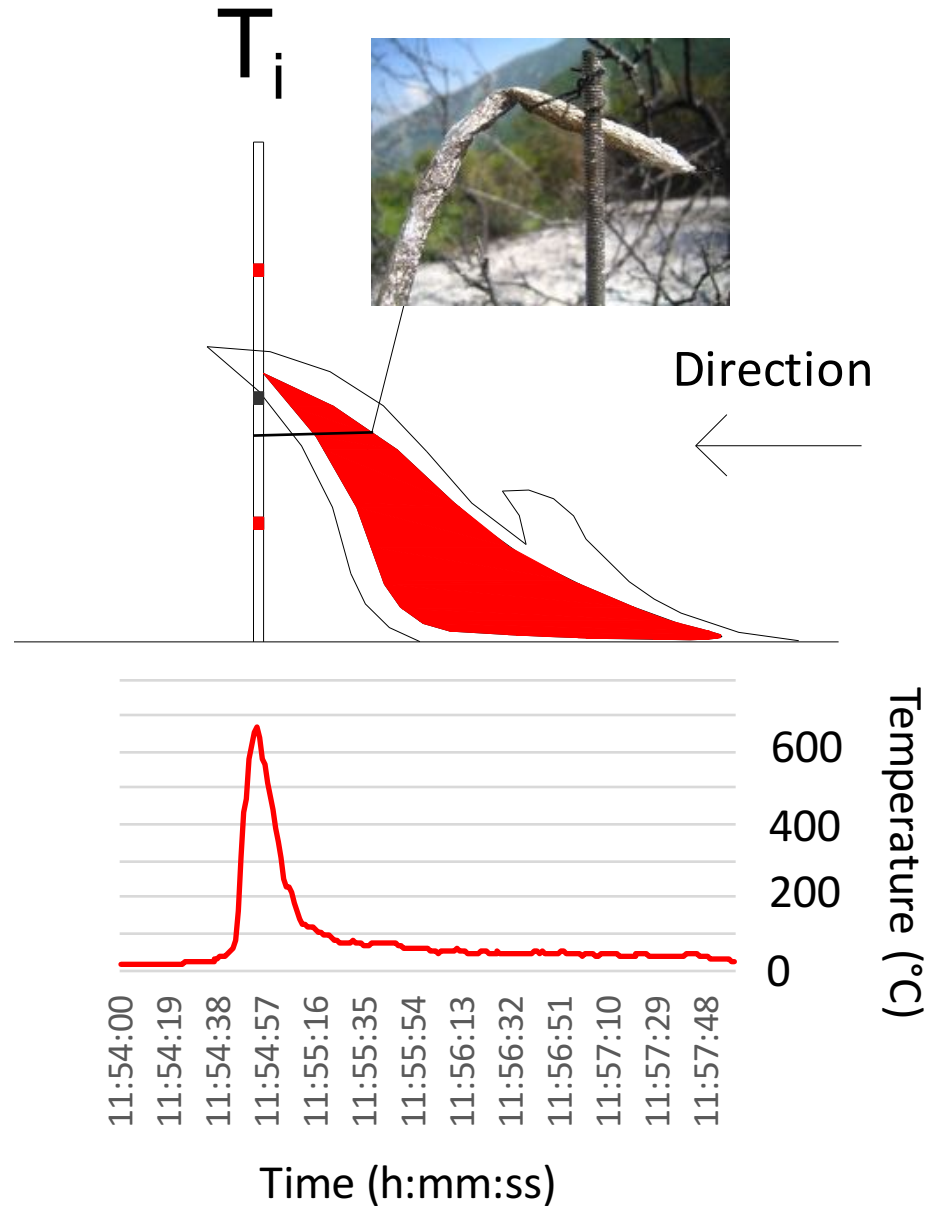
○ Marked points



Rate of spread: thermocouples



○ Marked points



Temperature and heat flux



Heat flux-meter



Thermocouple

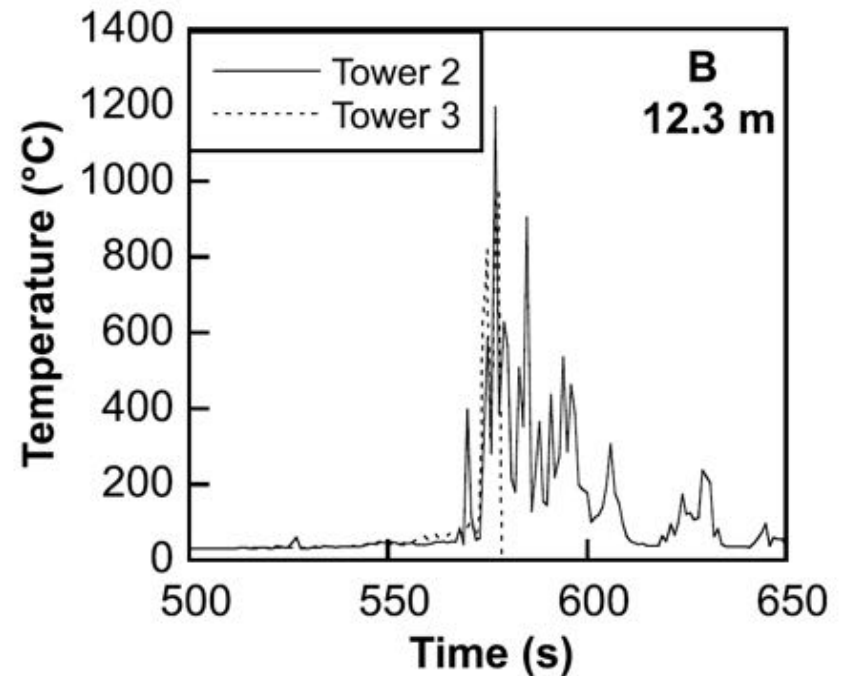
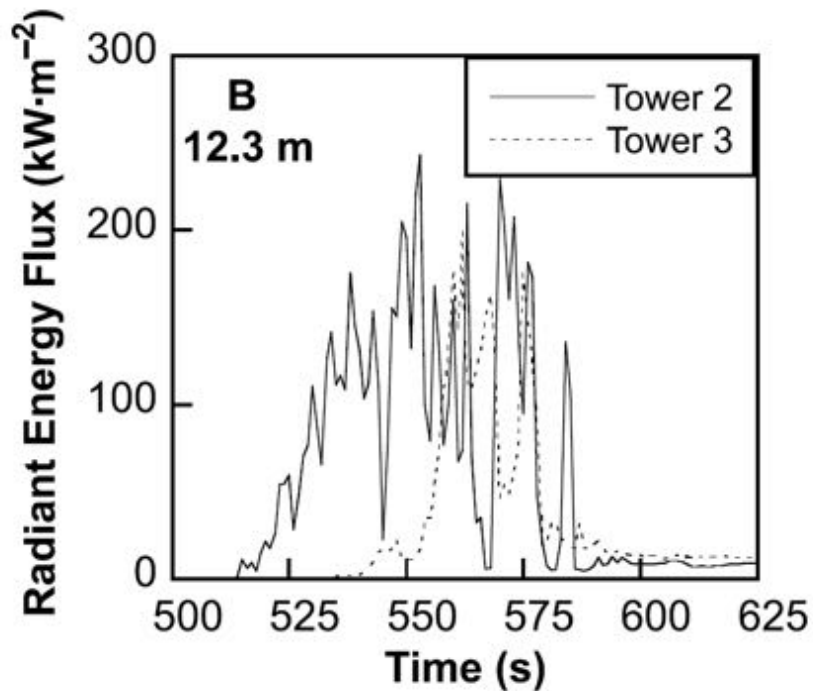


Data-logger



Source: Frédéric Morandini et Xavier Silvani

Temperature and heat flux



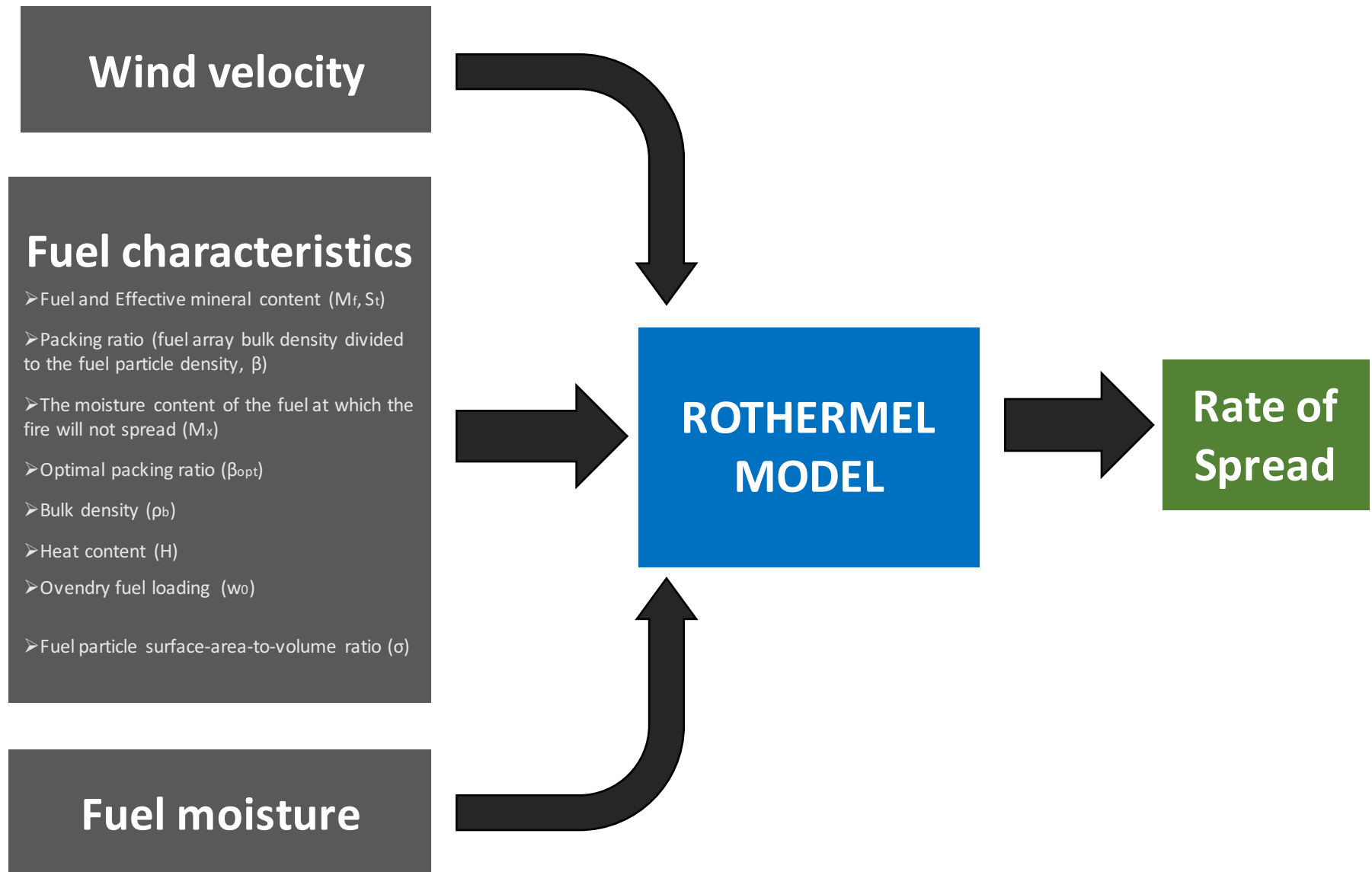
Butler B.W. et al. 2004
Measurements of radiant emissive
power and temperatures in crown fires
Canadian Journal of Forest Research
34(8): 1577-1587

Summary



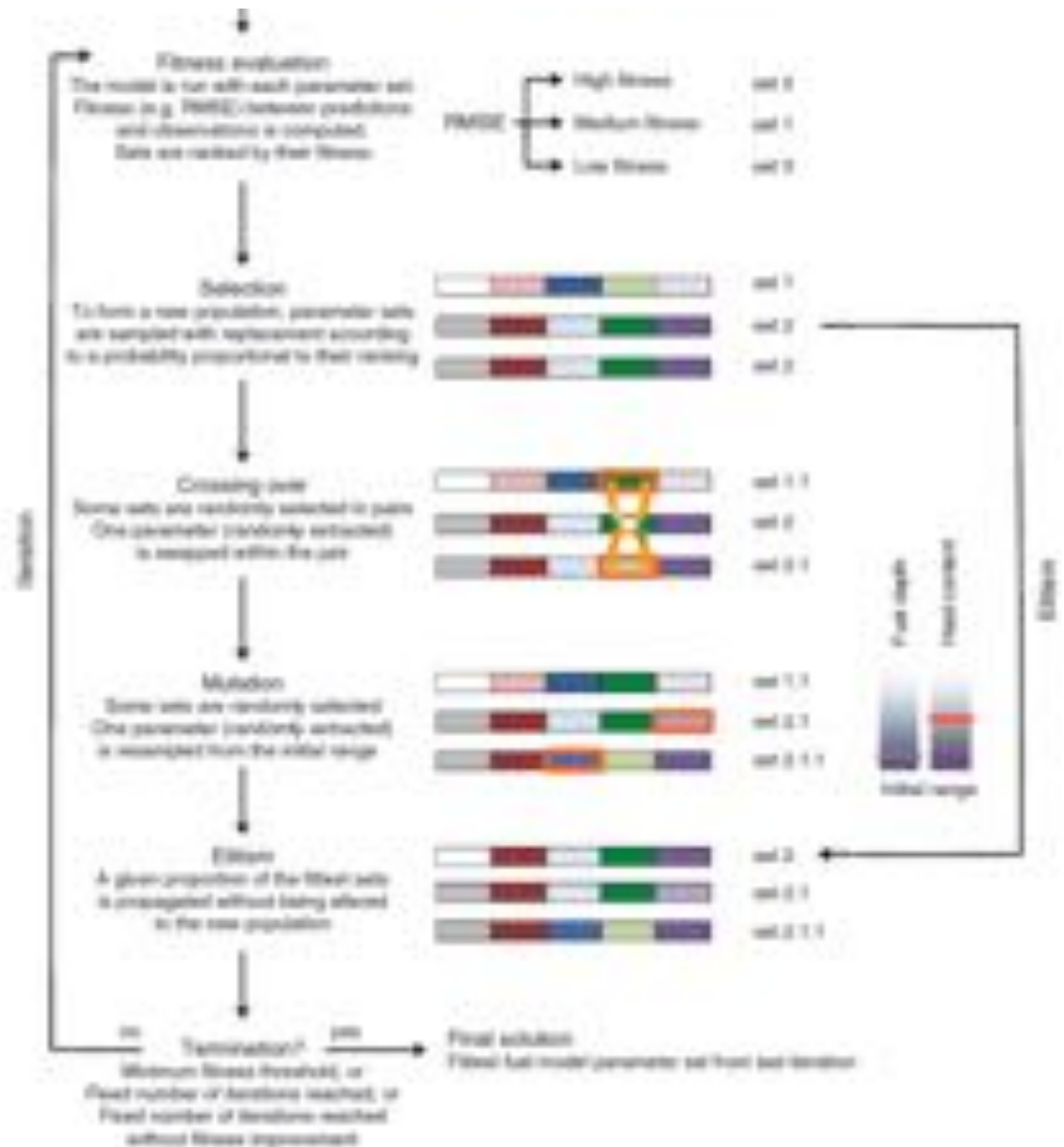
1. Why fire evolution modelling
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Rothermel model

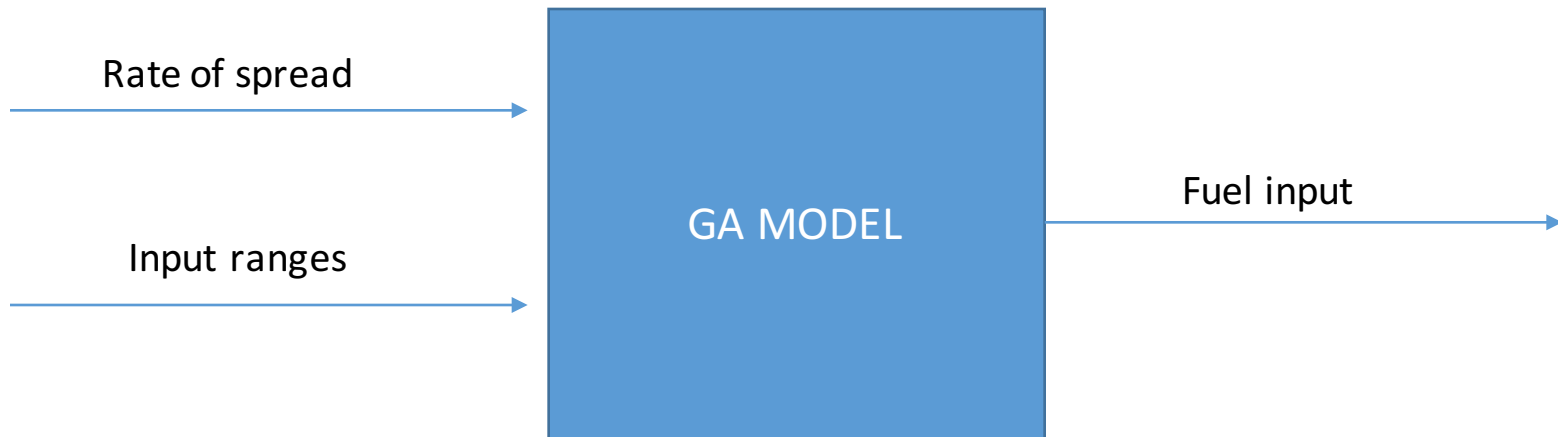
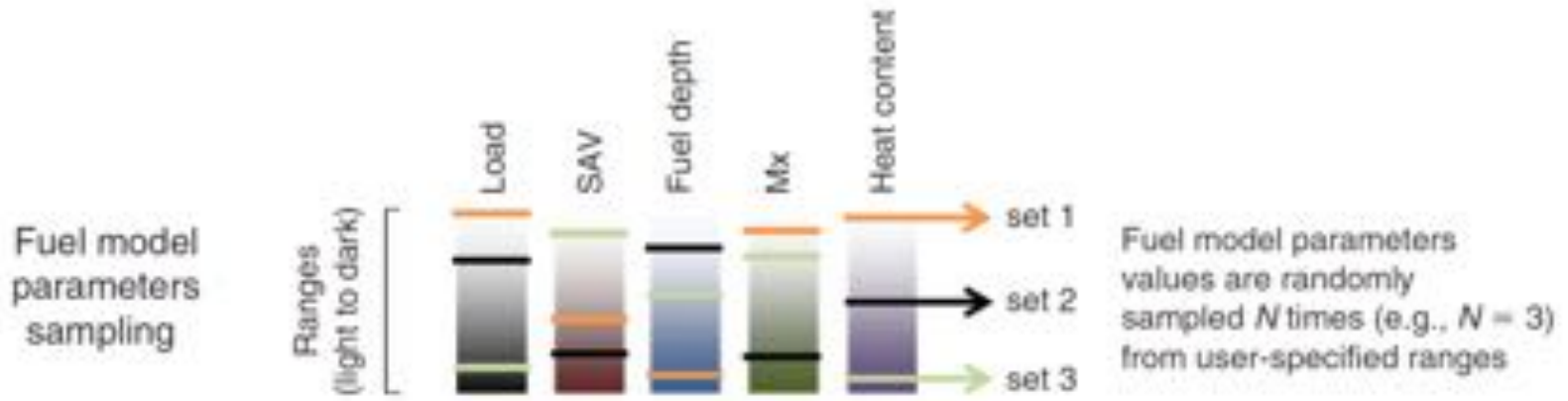


Genetic algorithm

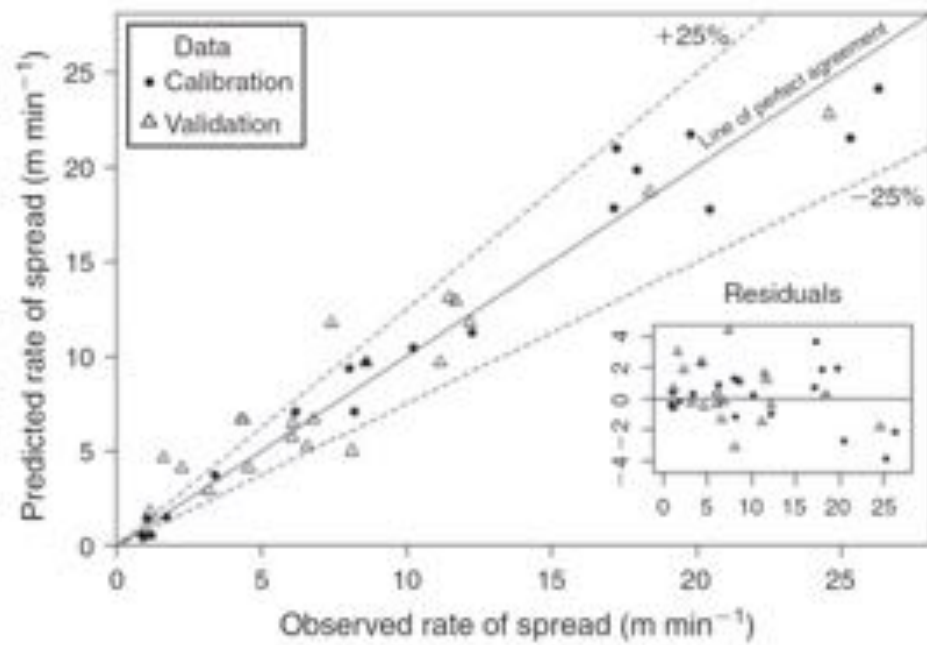
Initial population



GA for fuel model



Results



Results

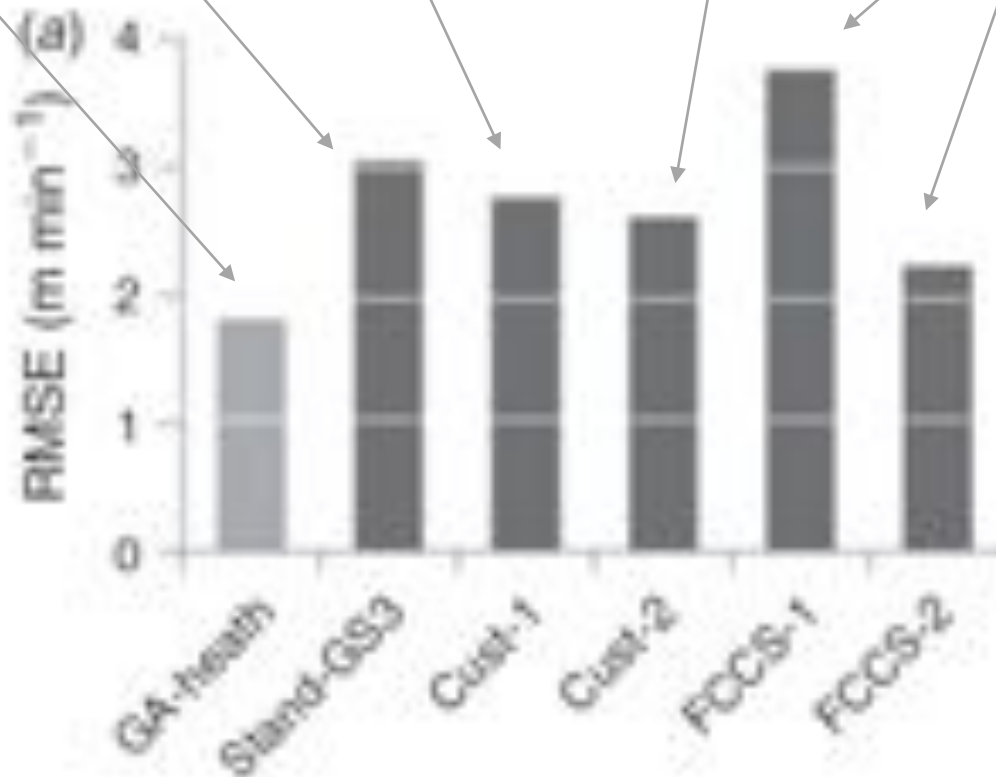
Rothermel calibrated using GA optimisation

Standard Rothermel fuel model

custom fuel model parameterised by averaging fuel characteristics

Site-specific custom fuel model parameterised by averaging fuel loadings and structure measured at each fire site

Rothermel model reformulation that is implemented in the Fuel Characteristics Classification System (Sandberg *et al.* 2007; Prichard *et al.* 2013).

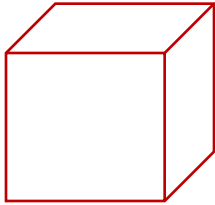


Summary



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1D physical model



$$\rho c \frac{\partial T}{\partial t} + k_v \frac{\partial T}{\partial x} = k \frac{\partial^2 T}{\partial x^2} - h(T - T_c) - \frac{H}{s} \frac{dM}{dt} + \Phi_{RAD}$$

$$\frac{dM}{dt} = -aM$$

$$\Phi_{RAD} = \sum_j r F_{ij} \epsilon \sigma (T_j^4 - T^4)$$

ENERGY AND MASS CONSERVATION
EQUATION APPLIED TO A CONTROL
VOLUME

Symbol	Explanation	Evaluation
P	Mixture air fuel density	Laboratory Analysis
C	Specific heat	(Campbell, Norman 2012)
k_v	Advective coefficient	GA using Thermocouple Measurements
K	Diffusive coefficient	GA using Thermocouple Measurements
h	Losses coefficient	GA using Thermocouple Measurements
H	Energy content	Laboratory Analysis
S	Fuel height	Field Analysis
A	Mass rate variation coefficient	GA using Thermocouple Measurements
R	Radiative coefficient	GA using Thermocouple Measurements

Experimental data



- Wind velocity and direction data are collected every 10 s

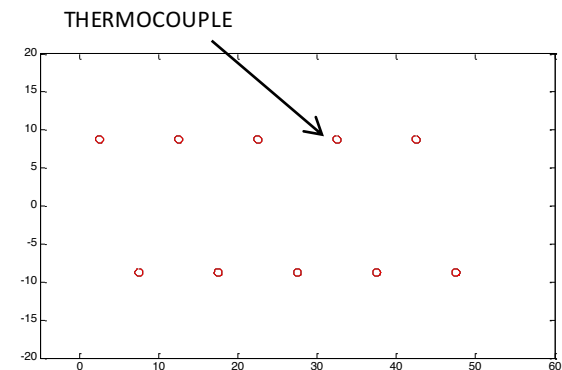
- Thermocouples detect temperature evolution during each experiment

- 4 Field experiments are carried out in different wind conditions

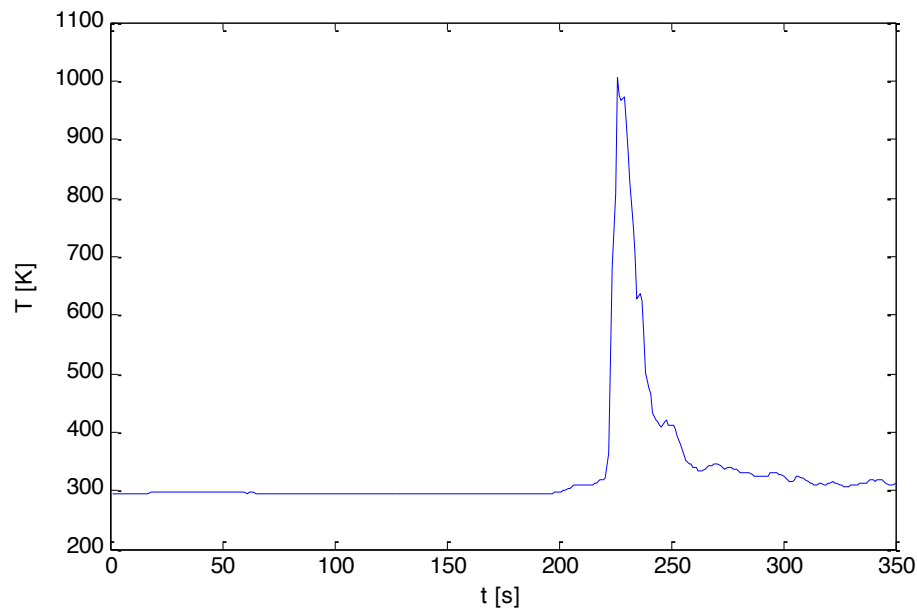
- Dead fully cured grasses (diameter < 6 mm). From laboratory and field analysis:

- Load $0,43 \text{ kg/m}^2$
- Height 10 cm
- Packing Ratio $0,002$
- Burned biomass $0,39 \text{ kg/m}^2$
- Bulk density 5 kg/m^3

- Heat power of fuel $18,5 \text{ MJ/kg}$
- Humidity 11% of dry fraction



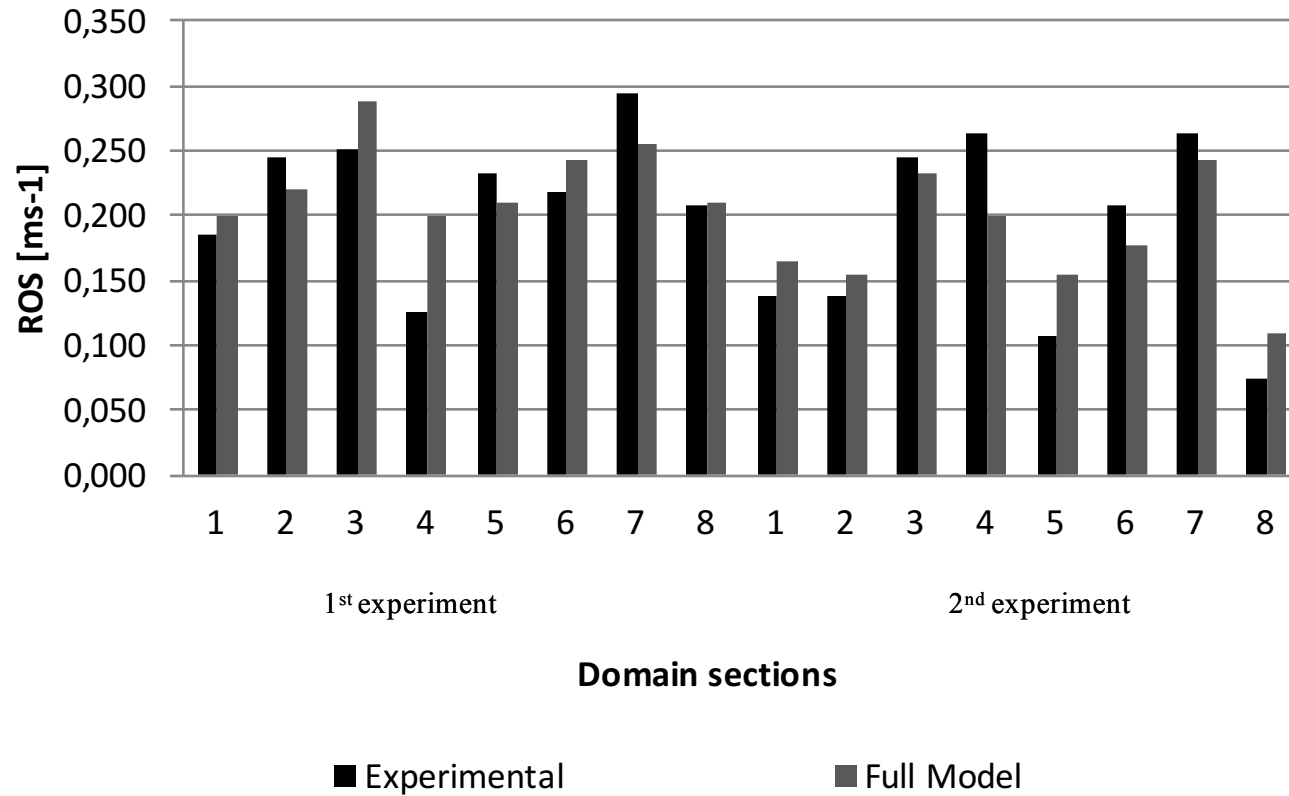
Model calibration through experimental data



$$Err = w_1 * Err_{max T} + w_2 * Err_{integral} + w_3 * Err_{arrive} + w_4 * Err_{burning}$$

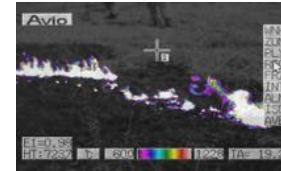
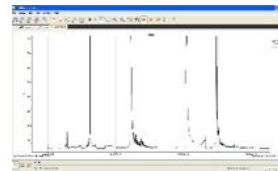
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Model calibration through experimental data



Thank you for the attention

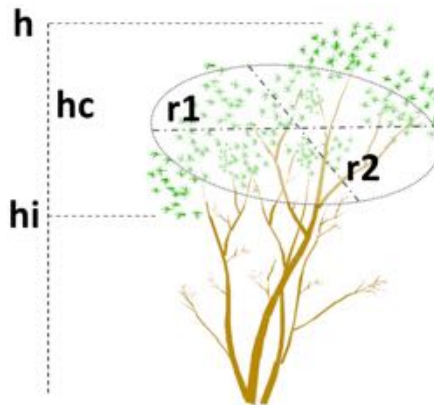
Davide Ascoli (Università di Napoli Federico II)
Elisa Guelpa (Politecnico di Torino – Dip. Energia)
Vittorio Verda (Politecnico di Torino – Dip. Energia)



What to measure?

Fire environment

- Fuel structural characteristics: direct-indirect
- Fuel moisture: direct-indirect (eg fire danger index)
- Wind field (direction, speed)
- Air temperature – relative humidity
- Orography (slope, aspect, elevation)

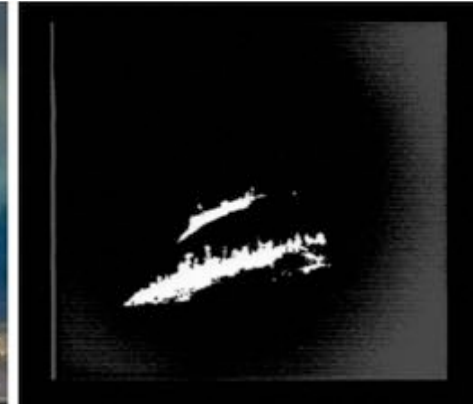


Exp. 7 – M1.3

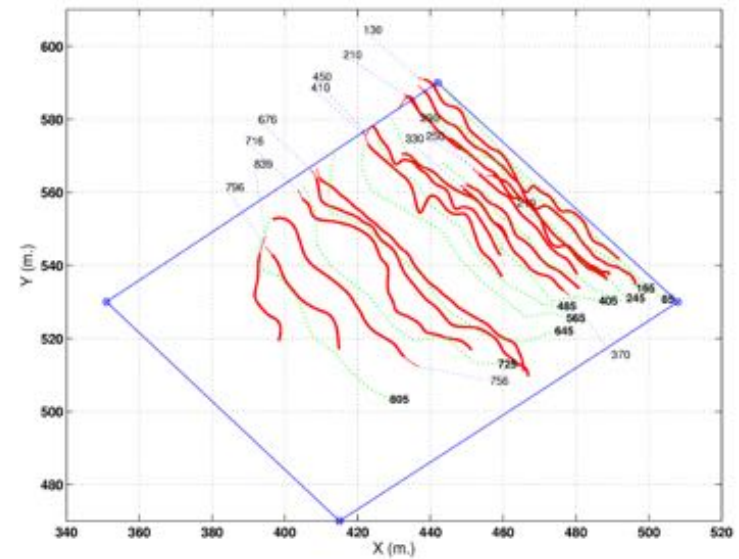
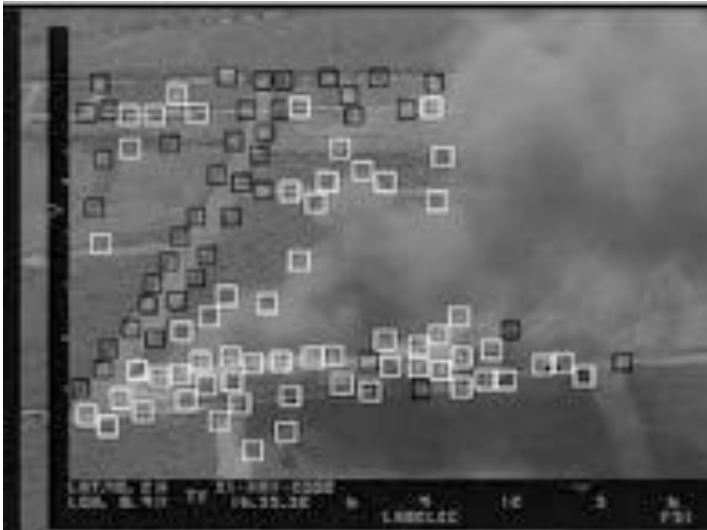
17.03.2005 12:01

Rate of spread: IR techniques

Ascoli - AFR3
Roma, 22 sept. 2016































Martinez-de-Dios et al. 2011



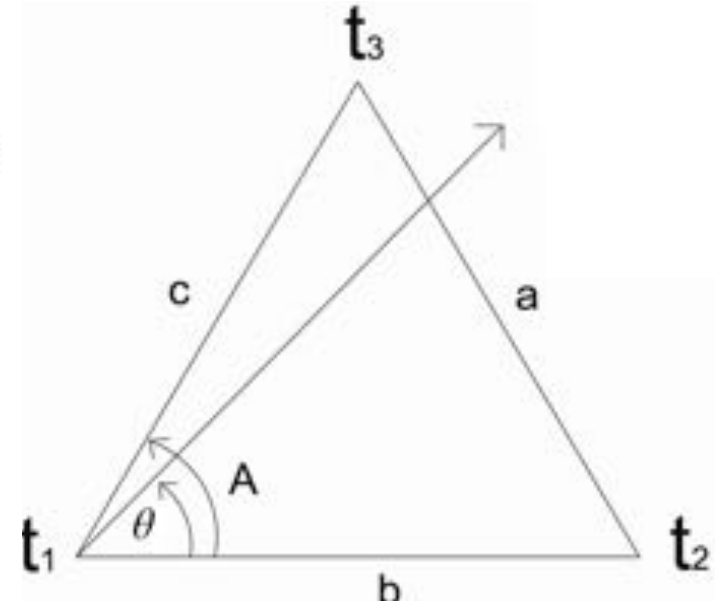
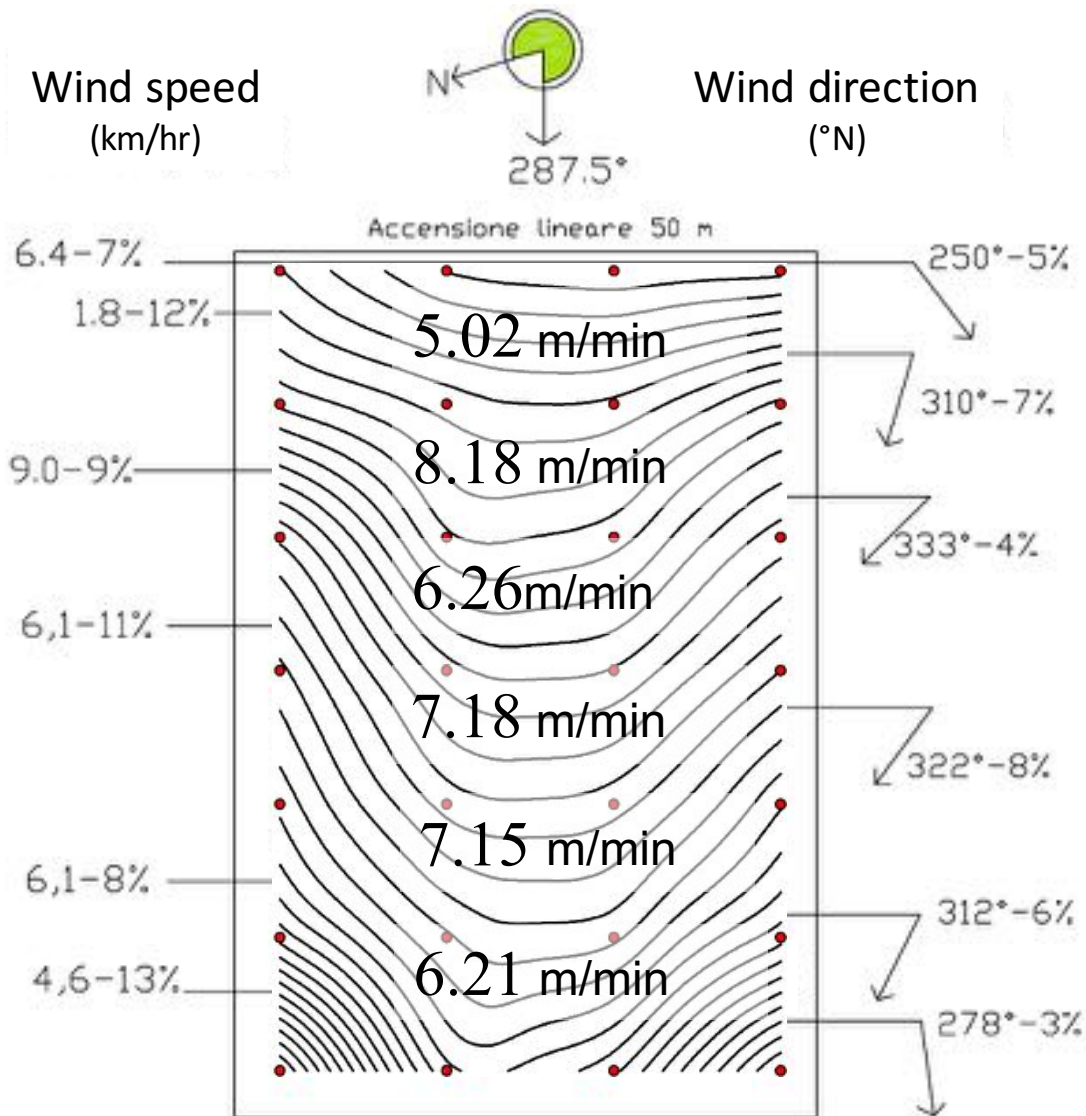
Rate of spread

Ascoli - AFR3
Roma, 22 sept. 2016

T4	T3	T1	T2
			
T8	T6	T5	T7
			
T14	T10	T9	T13
			
T20	T12	T11	T19
			
T24	T16	T15	T23
			
T27	T18	T17	T25
			
T28	T22	T21	T26
			

Rate of spread

Ascoli - AFR3
Roma, 22 sept. 2016



Fire Front Direction

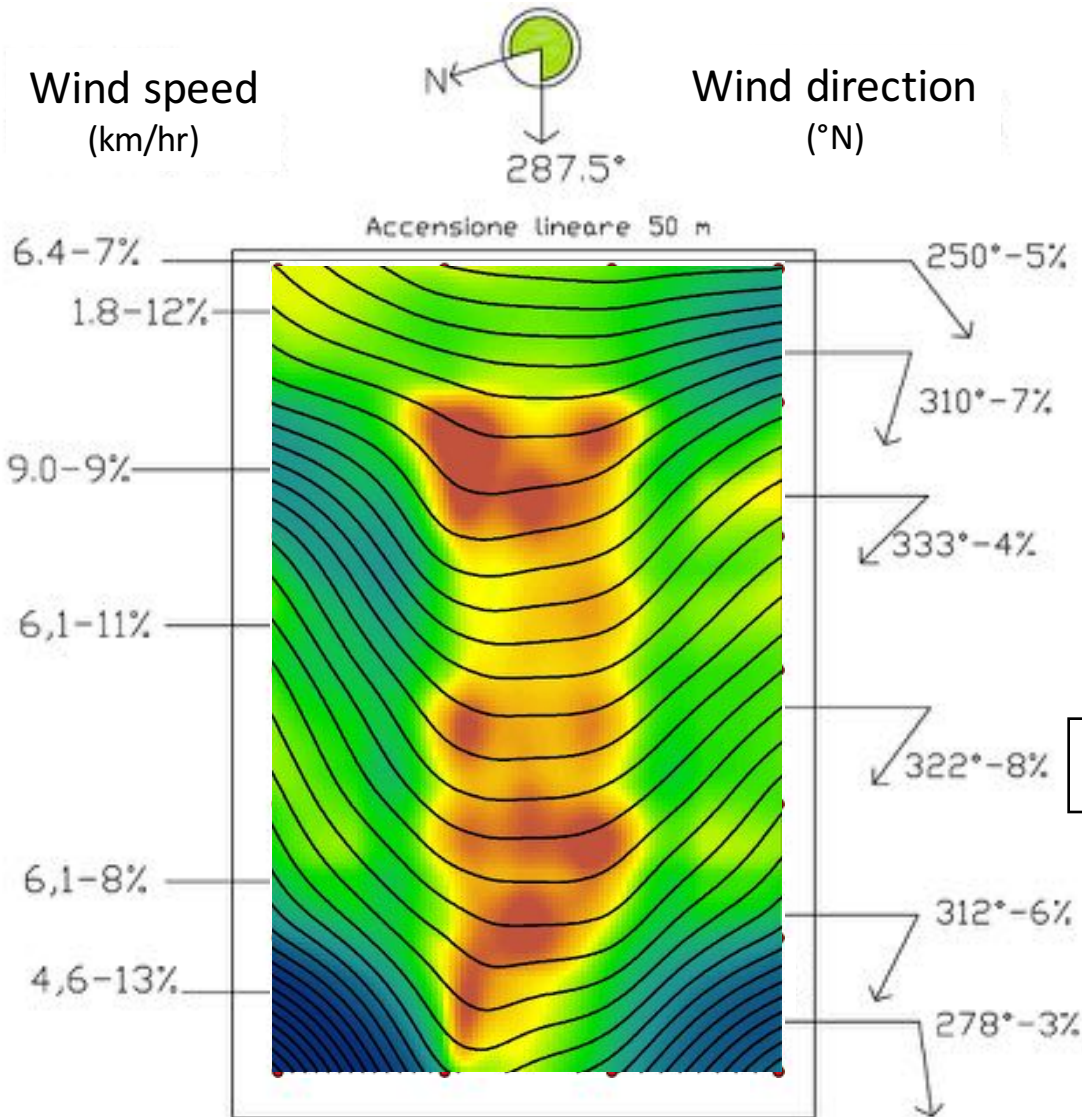
$$\Theta = \tan^{-1} \left[\left(\frac{t_3 - t_1}{t_2 - t_1} \right) \left(\frac{b}{c \sin A} \right) - \frac{1}{\tan A} \right]$$

Fire Rate of Spread

$$V = \frac{b \cos \theta}{t_2 - t_1}$$

Fireline intensity

Ascoli - AFR3
Roma, 22 sept. 2016



Fuel samples

$$\text{PRE} - \text{POST} = W \text{ (kg m}^{-2}\text{)}$$

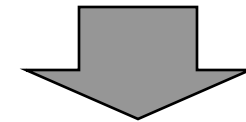
W = fuel consumed

X

ROS (m s⁻¹)

X

$$H = 18 \cdot 10^3 \text{ kJ kg}^{-1} \text{ heat content}$$



$$I_{\text{(kW m}^{-1}\text{)}} = \text{ROS} \times W \times H$$

Byram (1959)